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# Parameters Estimation at Ungauged Catchments Using Rainfall-Runoff Model, Upper Tekeze Basin, Ethiopia

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**Abstract:** This study was conducted for parameters estimation and stream flow prediction at ungauged catchments on the case of Upper Tekeze basin, Ethiopia by using Rainfall-runoff model. In the basin, most of the catchments were ungauged. The basin has 9199km<sup>2</sup> and 3638km<sup>2</sup> gauged and ungauged catchments respectively. Rainfall and stream flow data were analyzed in the period of 1992-2006 and 1992-20006, respectively. Parameters calibrated for gauged catchments were extrapolated to ungauged catchments on the base of similar physical catchment characteristics using regionalization techniques. Regionalization methods such as multiple linear regression, spatial proximity, sub basin mean and area ratio were applied to transfer model parameters values from gauged to ungauged catchments. For this study seven gauged catchments were satisfied objective functions in the calibrated and validation period, for example in Gheba catchment Nash-Sutcliffe model efficiency coefficient (NSE), relative volume error (RVE) and coefficient of determination (R<sup>2</sup>) were, 0.81, -4.25, 0.77 and 0.71, 5.5, 0.74 respectively. Stream flow simulation at ungauged catchments by using spatial proximity and sub basin mean method were contributing high runoff volume compare to other methods. The result for this study shows that the Key model parameters like runoff coefficient (Beta), recession coefficient of upper reservoir zone (Khq), Limit for evapotranspiration (Lp), field capacity (Fc), percolation (Perc) as defaulting value when applying HBV-96 model to the future regionalization studies. Model parameters were calibrated manually by try and error rules, however it was tedious therefore more creative automatic model calibration techniques could be useful for upcoming studies. Thus, Current and future water resources development endeavors may use apply such discharge data for planning and design purposes.

**Keywords:** HBV-96 Model, Parameter Estimation, Regionalization, Ungauged Catchment, Upper Tekeze Basin

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## 1. Introduction

Hydrological data are energetic for assessment of water resources problems, however most of Ethiopian river basins are ungauged. Poorly recorded and not well managed hydrological data that causes failure of most water and civil structures. This scarce hydrological data results uncertainty both in design and management of water resources system [11]. The situation in Upper Tekeze basin is more challenging there is no evenly distributed hydrometric stations and large areas have a lack of gauged stations and only a few years of data are available and recorded. Therefore it is better to understand the overall hydrological regime of the basin.

Models are used as utility of water resources development, in assessing and analyzing the available water resources, in studying the impacts of human interference in an area such as

land use land cover change, deforestation and other hydraulics structures such as dams and reservoirs [10]. Understanding the basic relationships between rainfall-runoff, soil moisture, ground water level and land use land cover is vital for an effective and sustainable water resources planning and management activities with the support of models [14].

Estimation of flow at ungauged catchments are often based on transferring information from gauged to ungauged sites by using area ratio, spatial proximity, sub-basin mean and regional model methods [18]. The most common approaches used for estimating flow at ungauged catchments is the use of conceptual rainfall-runoff models whose limits can be regionalized, with comparable catchment characteristics shows similar hydrological behaviors [14].

This regionalization method allows using the relationship

between model parameters and physical catchment characteristics of upper Tekeze basin by using HBV-96 model. The aim of this study was to simulate stream flow at ungauged catchments using rainfall-runoff models to solve water resource problems in the basin. Using few input variables such as rainfall, evapotranspiration, temperature, elevation zone, soil and land use land cover data to simulate stream flow at ungauged catchments in upper Tekeze basin.

In general stream flow simulation at ungauged catchments were important to asses surface and sub-surface water resource potential. Thus, simulated flows at ungauged catchments used for future water resources planning and design system in the basin yet.

## 2. Materials and Methods

### 2.1. Study Area Description

Tekeze river basin is located in the northwest of Ethiopia between 11°40' and 15°12' N latitude, and 36°30' and

39°50'E longitude. It is bordered by Mereb river basin and by Eritrea in the north, the Atbara river plains in Sudan in the west, Abbay river basin in the south and Danakil basin in the east. The basin has a total area of about 86,510 km<sup>2</sup>. But the study area has total area of 45580 km<sup>2</sup>. Elevation of the basin 500 low land and 3000 highland and 4620m above mean sea level on Mount Rash Dasha. Annual rainfall is 600 mm in the lowlands and 1,300 mm highland. Minimum and maximum Temperature is 32°C and 19-43°C. In upper Tekeze basin catchment characterized by seven major soil groups those are chromic Vertisols, Eutric Leptosols, Eutric Cambisols, Eutric Regosols, Eutric Fluvisol and Eutric Nitosol. Major land use land cover data of the catchment was characterized by annual crop, bar soil, closed shrub, moderate forest, perennial crop, wood land, Open grass, closed grass, sparse forest, open shrub and water body. The study area has 45,580km<sup>2</sup> among these the basin has 9199km<sup>2</sup> and 3638km<sup>2</sup> gauged and ungauged catchments.

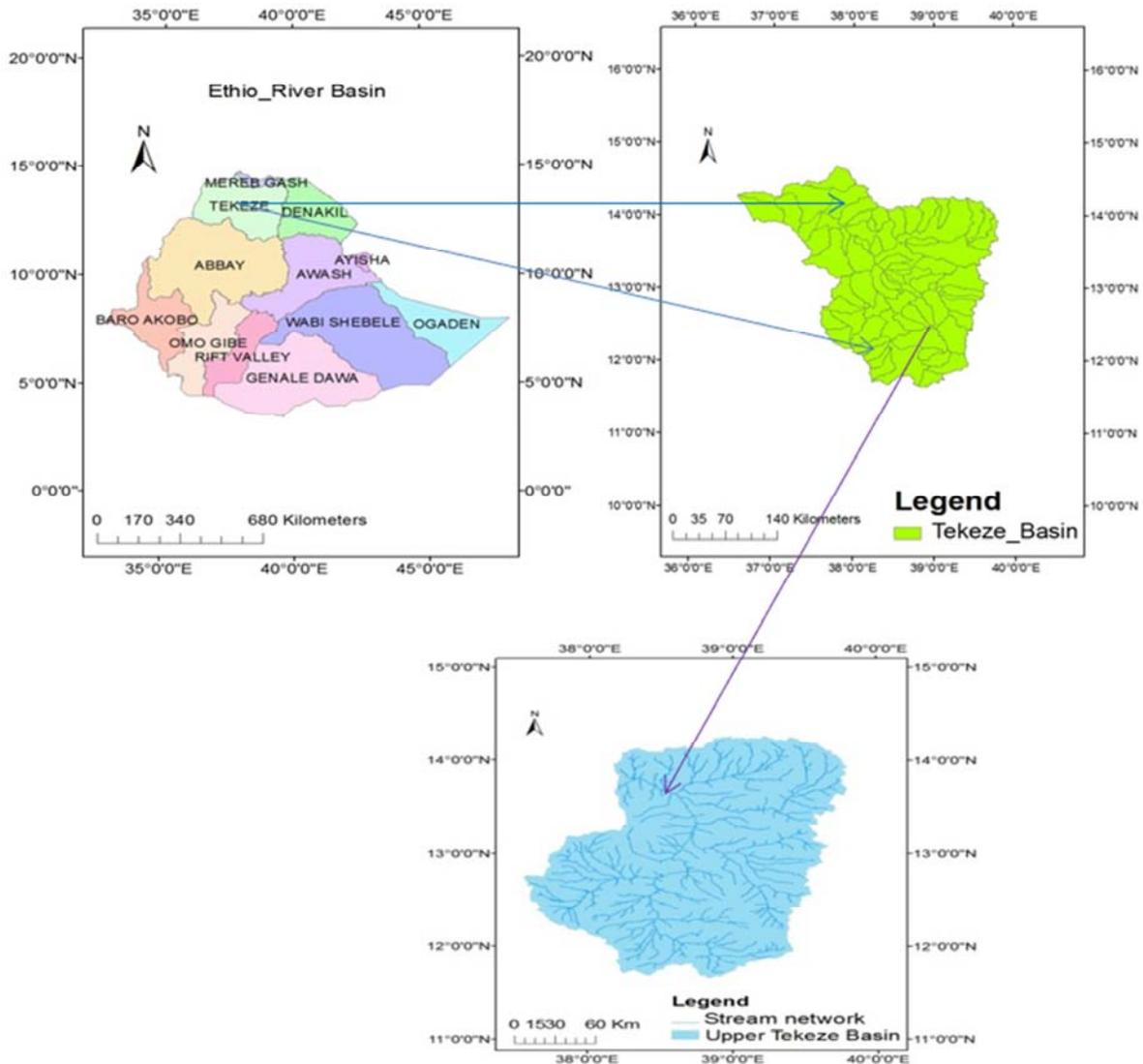


Figure 1. Location of the study area.

## 2.2. Data Collection

Depending on the availability and suitability of hydrological stations, stream flow from 1992-2006 years data collected from Ministry of Water, Irrigation and Electricity (MoWIE) under Hydrology department for model calibration and validation. Daily rainfall from 16 years (1992-2006) data were collected from National Meteorological Agency (NMSA) and 30\*30 DEM, LULC and soil data are used for identification of physical catchment characteristics both gauged and ungauged catchments from Ministry of Water, Irrigation and Electricity (MoWIE) under GIS department.

## 2.3. Analysis of Hydro-Meteorological Data

After selection of representative sites and collecting the required data for the model, missing rainfall and flow data were field using station average, normal ratio and regression

equations respectively. The data continuity and consistency were checked, therefore the bar graphs annual rainfall during 1992-2006 periods along with the 16-year mean rainfall were plotted to explore the annual rainfall pattern over the study area and then using double mass curve analysis to check homogeneity and consistency of rainfall as well as adjustment of inconsistent data.

Evapotranspiration was calculated by using Penman-Monteith and Hargreaves methods depending on the availability of data. However, Penman-Monteith method is recommended as the lone method for determining reference evapotranspiration (ET<sub>o</sub>) when the standard meteorological variables including air temperature, relative humidity and sunshine hours data are available [15]. Since some of meteorological stations had maximum and minimum temperature. Therefore, it was recommended to use Hargreaves method.

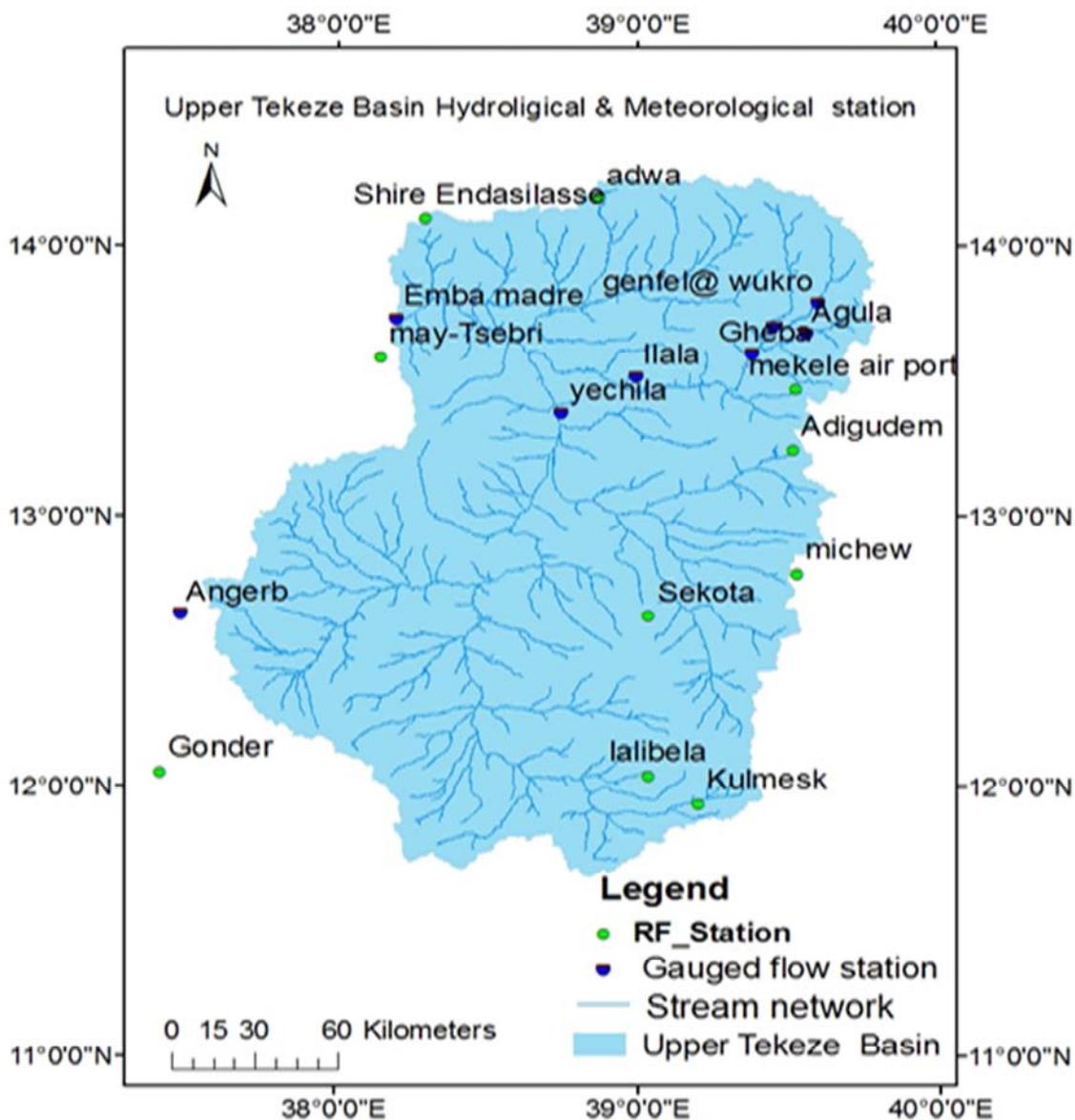


Figure 2. Location of Hydro-Meteorological stations.

**2.3.1. Catchment Delineation and Selection of Representative Catchments**

There are 39 gauged stations in the catchment however, seven gauged catchments were selected based on the availability of daily time series river flow data.

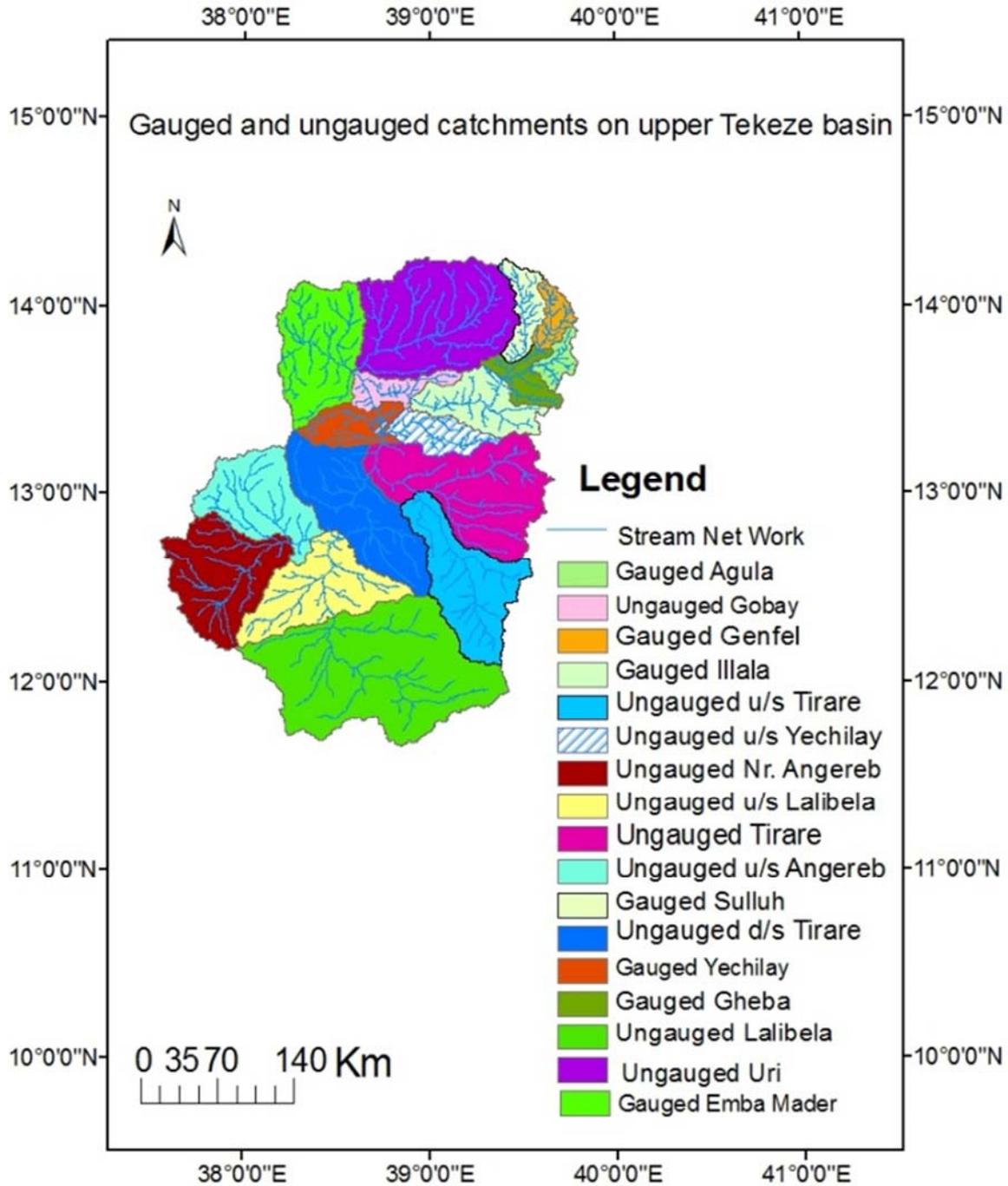


Figure 3. Gauged and ungauged major tributaries of upper Tekeze sub-basin.

**2.3.2. Selection of Representative Physical Catchment Characteristics**

Runoff generation is governed by physical catchment characteristics both gauged and ungauged catchments. In upper Tekeze basin a SRTM DEM 30\*30m resolution has been used to delineate catchments of the study area by using Arc GIS and Soil and Water assessment Tool (SWAT) with

GIS interface software. Selected catchment characteristics were used to develop methods to estimate stream flow characteristics for ungauged catchments. Physical catchment characteristics both gauged and ungauged catchments were identified that are overbearing for regionalization process such as geography, physiographic, soil type, land use and land cover and geology data [8].

### 2.3.3. Model Sensitivity Analysis

Sensitivity analysis was performed for each calibration event by varying each of the above parameters by plus or minus 20%, 40%, 60%, 80% etc., in separate simulations, and then calculating the percentage change in output parameters at a time [1]. Those model parameters having steep slope are considered as most sensitive whereas those having moderate to gentle slopes are considered as less sensitive.

### 2.3.4. Model Calibration and Validation

The applicability of the model should be evaluated through the process of sensitivity analysis, calibration and validation for further analysis of the result [17]. Calibration is carried out by trial-and-error procedure whereas model parameters are manually or automatic calibration. However, in this study manual calibration method was used a period 1993-2002 for calibration and 2003-2006 for validation with one year warm up period from 1992-1993. By changing one model parameter at a time until observed flow match with simulated stream flow.

### 2.3.5. Model Performance

For this study the model performance was evaluated by Nash-Sutcliffe model efficiency coefficient (NSE), coefficient of determination ( $R^2$ ) and relative volume error (RVE) for HBV -96 model for the calibration and validation period.

### 2.3.6. Checking the Model Performance

Simulate stream flow at ungauged catchments are important to check the model performance. For this study take three gauged catchments such as Emba Mader, Illala and Gheba let ungauged and transfer model parameters from four gauged catchments like Yechilay, Sulluh, Genfel and Agula using regionalization technique and simulate flow at ungauged catchments. Finally compare simulated and observed flow; if the simulated and observed flows are highly correlated to each other the model has best performance otherwise the reverse is true.

### 2.3.7. Regionalization

Regionalization is the process of transferring information from comparable catchments to the catchments of interest [3]. To generate flow at ungauged catchments it is vital to use regionalization to transfer information from gauged to ungauged catchments. Stream flow simulation needs a model parameters optimization for gauged catchments by fitting the observed and simulated stream flow [6]. For this study four regionalization methods are applied those are:

a) *Regional model*: Catchments for which flow time series are to be estimated may not have comparable gauged catchments [2]. Therefore, the methods of regionalization using similarity of catchment characteristics of regional model were applied to estimate the flow of ungauged

catchments [12]. Each model parameters estimated by regional model was resulting using equation.

b) *Spatial proximity*: choice of catchments information is to be transferred gauged to ungauged site is usually based on similarity of catchment characteristics measure. This method is based on the underlying principle that catchments that are close to each other will likely have a similar runoff regime since climate and catchment conditions will often only vary marginally in space [9]. Catchments are highly homogeneous with respect to topographic and climatic properties that means land cover, soil, geology and physiographic and climate physical catchment characteristics [16].

c) *Area ratio*: Optimized model parameters of gauged catchments are directly transferred to ungauged catchments of equivalent area based on the assumption that catchment area is the dominant factor for controlling the volume of water that can be generated from the rainfall. If the area ratio between gauged and ungauged catchments is greater than 50%, the model parameters of gauged catchments are not transferred to ungauged catchments [5].

d) *Sub-basin mean*: sub-basin mean represents the arithmetic mean of calibrated model parameter sets of gauged catchments that fulfill the objective functions [7].

### 2.3.8. Establishing the Regional Model

In order to set up a regional model to predict the model parameters in ungauged catchments, a statistically significant relationship established between Physical catchment characteristics and calibrated model parameters by using excel in data analysis. After determining the model parameters through model calibration and selection of physical catchment characteristics, a method for establishing the relationship is applied [13].

### 2.3.9. Estimation of Model Parameters and Stream Flow Prediction at Ungauged Catchments

After determining simple linear relationships between model parameters and physical catchment characteristics, optimizing by multiple regressions analysis for several physical catchment characteristics. The main objective is that select relationships that are acceptable and statistically significant.

## 2.4. Spatial Temporal Data

### 2.4.1. Topographic Map

SRTM  $30 \times 30$  DEM was downloaded from earth explorer. The upper Tekeze catchments was extracted from Ethiopian DEM.

### 2.4.2. Land use Landcover Map

From ERDAS 2008 LULC map for the study is the generated classification are as follows Shrub land, Cultivation, bare land, woodland, waterbody, plantation, natural forest and grass land etc.

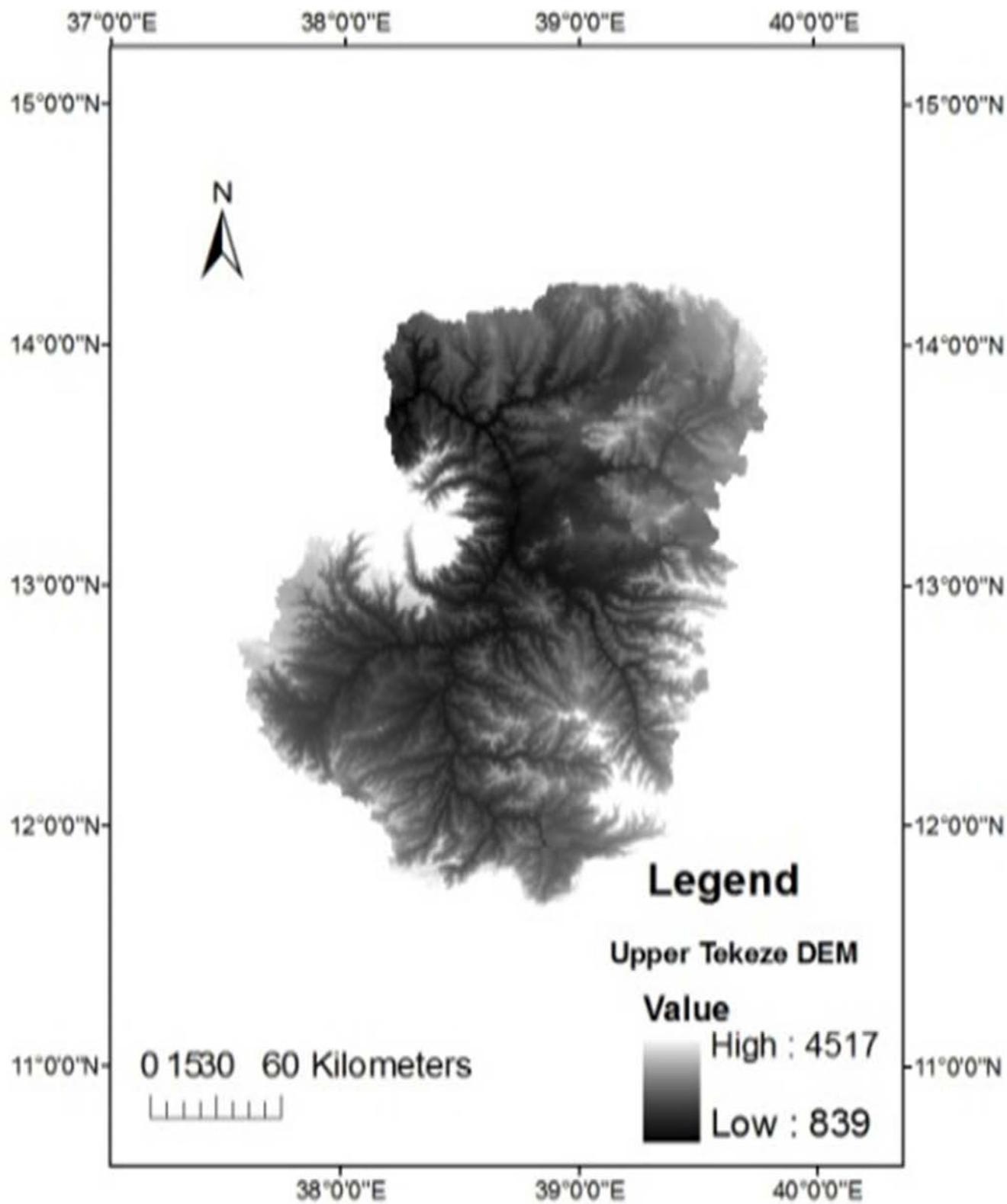


Figure 4. SRTM 30\*30 DEM of upper Tekeze basin.

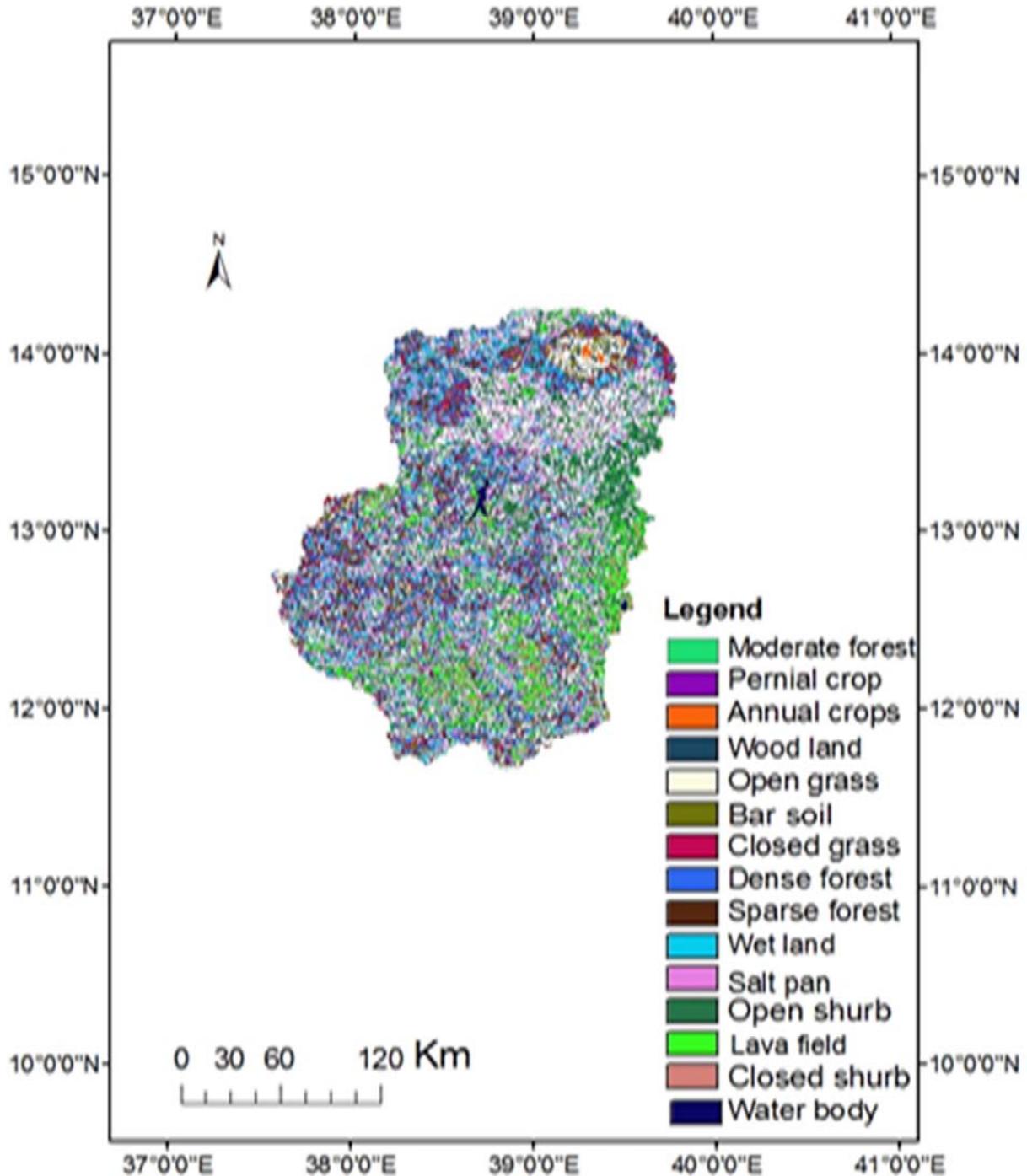


Figure 5. Land use land cover map of the study area.

## 3. Results and Discussions

### 3.1. Model Development HBV-96

#### 3.1.1. Sensitivity Analysis

For this research work sensitivity analysis, like runoff coefficient (Beta), recession coefficient of upper reservoir zone (Khq), percolation (Perc), Limit for evapotranspiration (Lp) and field capacity (Fc) were more sensitive model parameters, whereas recession coefficient for lower reservoir

( $K_4$ ), capillary rise coefficient (cflux) and response routine (Alfa) are relatively less sensitive for upper Tekeze sub-basin. For this research work model parameters such as response routine (alfa), capillary rise coefficient (cflux) and recession coefficient for lower reservoir ( $K_4$ ) do not show significant effect on the model performance, however, for other researchers' such as Bishaw, (2012), Birhane, (2013) and Tesfaye, (2011) analysis model parameters like lower reservoir ( $K_4$ ) and response routine (Alfa) shows significant effect [4]. For this study sensitivity analysis of Emba Madre sub basin as shown below.

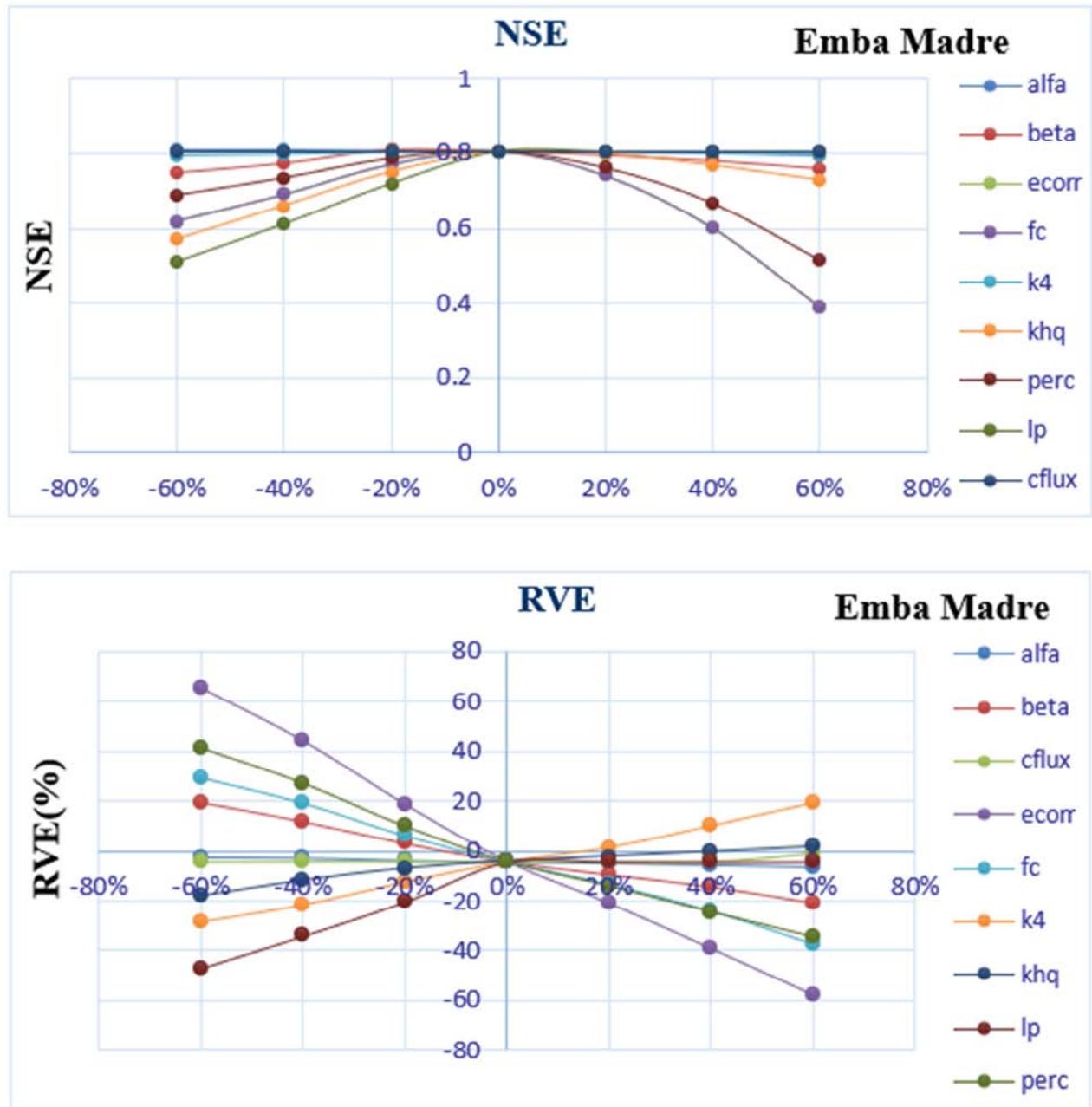


Figure 6. Sensitivity analysis of Emba Madre sub basin.

**3.1.2. HBV Model Calibration and Validation Results**

Ten years from period 1993-2002 for calibration which includes one years of warm up period and for the validation from 2003-2006 for validation with one year worm up period from 1992-1993. The model performance of Emba Mader watershed by HBV-96 model are satisfactory with objective functions like Nash-Sutcliffe model efficiency coefficient (NSE)=0.7, coefficient of determination ( $R^2$ )=0.8, relative volume error (RVE)=4.8 and Nash-Sutcliffe model efficiency coefficient (NSE)=0.88, coefficient of determination ( $R^2$ )=0.74, relative volume error (RVE)=-4.1 for the calibration and validation period respectively.

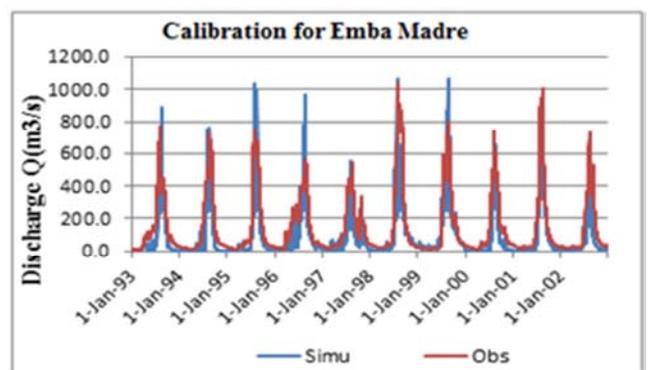


Figure 7. Observed and simulated discharge during calibration period.

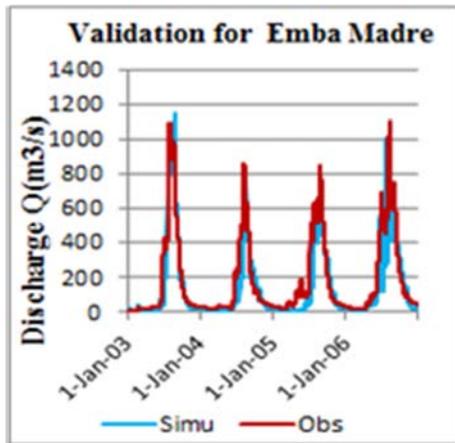


Figure 8. Observed and simulated discharge during validation period.

### 3.2. Result of Regionalization

#### Checking Model Performance

This research work is not only predicting stream flow at ungauged catchments however, before simulate stream flow at ungauged catchments it is important to check the model performance. For this study take three gauged catchments like Emba Mader, Illala and Gheba let ungauged and transfer model parameters from four gauged catchments like Yechilay, Sulluh, Genfel and Agula using regionalization technique and simulate flow at ungauged catchments. Finally compare simulated and observed flow; if the simulated and observed flows are highly correlated to each other the model has best performance. Following this procedure simulated and observed flow are fitted or best correlated this shows that HBV-96 model has good performance for simulation of steam flow. Especially stream flow computed by multiple linear regression method and observed flow are best correlated to each other; therefore, multiple linear regression method is best compared to others methods. However, other researchers don't check the model performance rather than simulating stream flow for ungauged catchments.

To check the model performance simulated and observed

flow comparison of Emba Madre sub catchment was shown in the figure 9 bellow. The results show that the model is reasonably well performed with coefficient of determination ( $R^2$ ), Nash-Sutcliffe model efficiency coefficient (NSE) and relative volume error (RVE) are 0.78, 0.76 and 2.6 respectively.

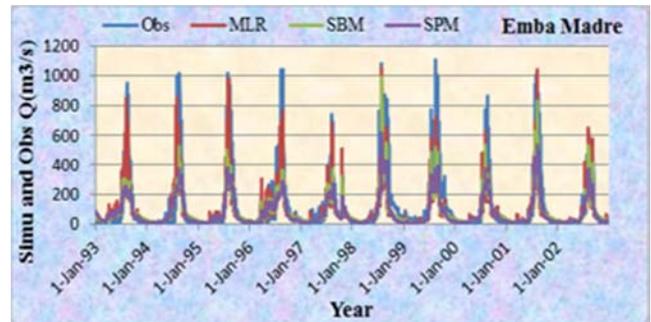


Figure 9. Comparison of observed and simulate flow.

From the above graph simulated flow by multiple linear regression method and observed flow are best correlated to each other; therefore, multiple linear regression method is best comparing to others methods, however in this study multiple linear regression model is the best method it is not contribute high runoff volume however, some researcher's multiple linear regression model contributes high runoff volume compare to other methods. For the next study each regionalization method must be clearly identified and the model performance must be checked.

### 3.3. Multiple Linear Regressions Results

The relationships between physical catchment characteristics and model parameters were assessed through multiple linear regression analysis. Depending on the coefficient of determination ( $R^2$ ) ( $\geq 0.85$ ) and significance or p-value ( $\leq 0.10$  for 95% confidence interval) physical catchment characteristics were selected to establish regression equations.

Table 1. The regional model for model parameters and physical catchment characteristics links.

Coefficients	95% confidence interval			P-value	Lower Bound	Upper Bound	Co-linearity $R^2$
	Model Parametres	Std Error	t-stat				
<i>Alfa</i> = $B_0+B_1*chromic\ cambisol+B_2*barsoil$							
$B_0$	0.5069	0.0360	14.0651	0.0008	0.3922	0.6216	0.94
$B_1$	0.0066	0.0010	6.6432	0.0070	0.0034	0.0097	
$B_2$	-0.0135	0.0032	-4.2060	0.0245	-0.0238	-0.0033	
<i>Beta</i> = $B_0+B_1*Nitsoil+B_2*ER$							
$B_0$	1.8281	0.5831	3.1355	0.0518	-0.0274	3.6837	0.97
$B_1$	0.0392	0.0060	6.5362	0.0073	0.0201	0.0582	
$B_2$	-0.2808	0.2599	-1.0804	0.3591	-1.1079	0.5463	
<i>Cflux</i> = $B_0+B_1*HI+B_2*Mpdry$							
$B_0$	0.9156	0.1628	5.6244	0.0111	0.3975	1.4337	0.97
$B_1$	-2.6794	0.3604	-7.4342	0.0050	-3.8264	-1.5324	
$B_2$	1.0183	0.0930	10.9488	0.0016	0.7223	1.3142	
<i>Ecorr</i> = $B_0+B_1*Shurb\ Land$							
$B_0$	0.1492	0.0145	10.2945	0.0005	0.1090	0.1894	0.85
$B_1$	-0.0014	0.0003	-4.5480	0.0104	-0.0022	-0.0005	

Coefficients	95% confidence interval					Co-linearity R <sup>2</sup>	
	Model Parametres	Std Error	t-stat	P-value	Lower Bound		Upper Bound
	Fc=B0+B1*Cambisol+B2*HI						
B0	4127.7966	1726.3586	2.3910	0.0751	-665.3432	8920.9365	0.82
B1	-5.2960	8.1468	-0.6501	0.5511	-27.9152	17.3233	
B2	-5010.6934	3198.6727	-1.5665	0.1923	-13891.6326	3870.2458	
	K4=B0+B1*Orthicsolonchaks						
B0	0.0087	0.0048	1.8087	0.1303	-0.0037	0.0210	0.91
B1	0.0045	0.0006	7.0625	0.0009	0.0029	0.0062	
	Khq=B0+B1*chromic cambisol+B2*Wet Land						
B0	0.0050	0.0160	0.3089	0.7776	-0.0461	0.0560	0.9
B1	0.0015	0.0003	5.1184	0.0144	0.0006	0.0025	
B2	0.0007	0.0003	2.9074	0.0621	-0.0001	0.0016	
	perc=B0+B1*Fluvsol+B2*Shurb Land						
B0	0.9929	0.2803	3.5419	0.0240	0.2146	1.7712	0.91
B1	-0.1183	0.0268	-4.4169	0.0115	-0.1927	-0.0440	
B2	0.0224	0.0050	4.4699	0.0111	0.0085	0.0363	
	lp=B0+B1*PET						
B0	1.6499	0.0292	56.4151	0.0000	1.5747	1.7251	0.99
B1	-0.0004	0.0000	-24.1895	0.0000	-0.0005	-0.0004	

**3.4. Determination of Model Parameters for Ungauged Catchments**

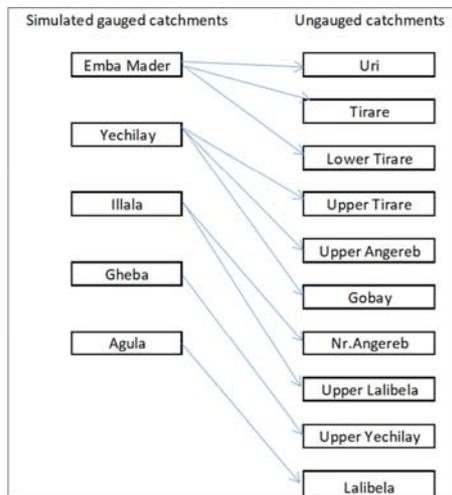
To determine model parameters for ungauged catchments seven flow gauged catchments like Emba Madre, Yechilay, Illala,

Genfel, Sulluh, Agula and Gheba and ten ungauged catchments were selected in upper Tekeze basin. Therefore, to determine model parameters of those ungauged catchments the following four methods were applied or used:

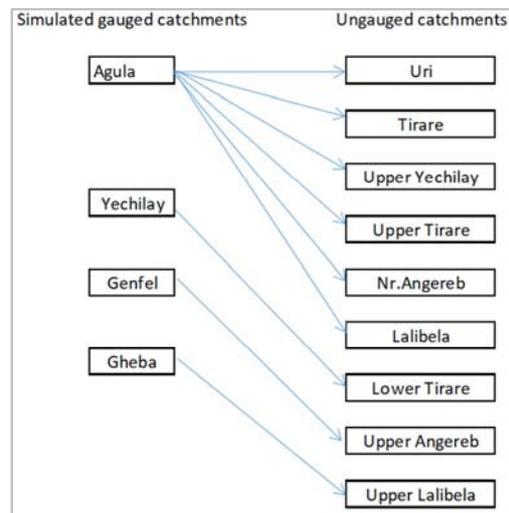
*Regional model method:* Each model parameters estimated by regional model was derived using equation (Table 1) above.

*Table 2. Model parameters estimated for ungauged catchments using regional model.*

Ungauged catchments	Alfa	beta	Cflux	Ecorr	Fc	k4	Khq	perc	Lp
Uri	0.505	1.64	-0.03	0.149	1409.76	0.010	0.005	0.995	0.982
Tirare	0.506	1.25	0.13	0.148	818.71	0.009	0.005	1.009	1.019
U/s Tirare	0.507	1.28	0.22	0.149	976.54	0.009	0.005	1.004	1.027
Lalibela	0.507	1.40	1.64	0.149	1148.19	0.009	0.005	1.000	0.557
U/s Lalibela	0.506	1.41	0.04	0.149	812.77	0.009	0.005	1.004	1.004
Nr. Angereb	0.506	1.30	0.08	0.149	1516.08	0.010	0.005	0.993	0.977
U/s Angereb	0.506	1.07	0.08	0.149	895.49	0.009	0.005	0.968	1.004
D/s Tirare	0.505	1.35	0.26	0.149	1275.11	0.009	0.005	0.984	1.018
U/s Yechilay	0.505	1.13	0.07	0.148	1502.91	0.009	0.005	1.005	1.009
Gobay	0.506	1.20	0.32	0.148	1084.40	0.009	0.005	1.002	1.002
Mean	0.506	1.294	0.22	0.148	1143.99	0.009	0.005	0.996	0.960



**Figure 10.** Model parameters transfer by spatial proximity method.



**Figure 11.** Model parameters transfer by area ratio method.

*Spatial proximity method:* Transferring model parameters from gauged catchments to ungauged catchments based on similarity of catchment characteristics (Figure 10) using spatial proximity Method. Similarity of catchment characteristics between gauged and ungauged catchments of upper Tekeze sub-basins are as shown below.

*Area ratio method:* In case of area ratio method Emba Madre model parameters is not transferring any ungauged catchments because area ratio between Emba Madre and those ungauged catchments are greater than 50%. Figure 11. shows that model parameters transferred from gauged to ungauged catchments based on area ratio method.

#### *Sub-basin mean method*

The average value of gauged catchments (Emba Madre, Yechilay, Illala, Genfel, Agula and Gheba) model parameters were taken for each ungauged catchment to simulate stream flow for ungauged catchments based on the principle of sub-basin mean method.

### 3.5. Simulation of Stream Flow at Ungauged Catchments

Model parameters estimated from ungauged catchments were simulated by HBV-96 model. Monthly average simulated flow for ungauged upper Tirare sub-catchments shown in the following Figure 12 in four methods i.e., Multiple Linear Regression (MLR), Sub basin mean (SBM), Spatial Proximity (SPM) and area ratio (AR) method.

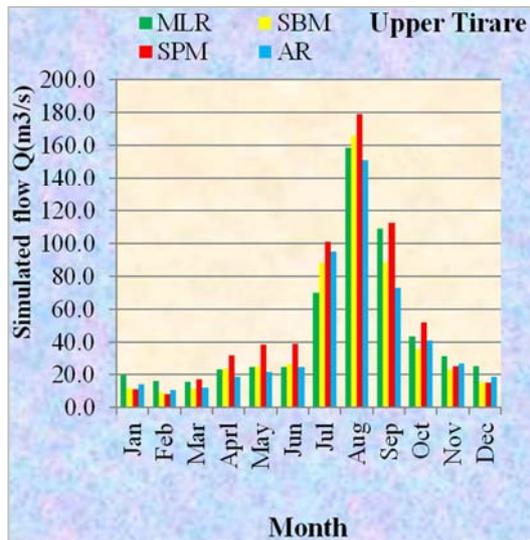


Figure 12. Monthly average simulated flow for selected sub catchments.

The above figure show that runoff simulated by spatial proximity and sub basin mean method contributes high runoff volume compare to other two methods. This implies that area ration method is poor because it is only considering the size between gauged and ungauged catchment areas. However, runoff estimated by multiple linear regressions are best fitted with observed flow, therefore this method is appropriate to predict discharge for ungauged catchments compare to other methods in upper Tekeze sub basins.

In this study multiple linear regression model is the best method it is not contribute high runoff volume however,

some researcher's analyze multiple linear regression model contributes high runoff volume compare to others methods. For next study each regionalization method must be clearly identified using syntiffic approach.

## 4. Conclusions

Based on the applied methodology and results obtained, the following conclusions are drawn:

In upper Tekeze sub-basin there are some gauging stations while seven of them have continuous river flow data from 1992 to 2006. Those have been simulated with a reasonable performance Nash-Sutcliffe model efficiency coefficient (NSE) greater than 0.60 and relative volume error (RVE) smaller than +10% or -10%.

Before simulating stream flow for ungauged catchments three best flow record gauged catchments lets assumed ungauged. Transfer model parameters from gauged to ungauged catchments and then simulate stream flow for those ungauged catchments. Finally compare simulated and observed flow by different methods in order to checking the model performance. For this study the model is well performed.

The model was calibrated and validated at gauged catchments from 1993 to 2002 and 2003 to 2006 respectively. Sensitivity analysis of HBV-96 model parameters was carried out manually by trial-and-error procedure.

According to sensitivity analysis, runoff coefficient (Beta), recession coefficient of upper reservoir zone (K<sub>hq</sub>), percolation (Perc), Limit for evapotranspiration (L<sub>p</sub>), and field capacity (F<sub>c</sub>) were more sensitive model parameters while recession coefficient for lower reservoir (K<sub>4</sub>), capillary rise coefficient (cflux) and parameters response routine (alfa), are relatively less sensitive for upper Tekeze sub-basin.

Model parameters for ungauged catchments are estimated by regional model, spatial proximity, catchment area ratio and sub-basin mean method. The model parameters of Emba Madre catchments were not transferred to any ungauged catchments since the area ratio between Emba Madre and ungauged catchments were greater than 50%.

For this study comparisons of regionalization methods indicate that stream flow simulation at ungauged catchments estimation by spatial proximity, sub basin mean and area ration method contributes high and less runoff volume respectively. Therefore for upper Tekeze sub-basin multiple linear regression method is best compare to other methods. Generally, in upper Tekeze river basin HBV-96 model is found to be acceptable results for estimation daily stream flow at ungauged catchments.

## 5. Recommendations

The following recommendations are given on the basis of the next research work on upper Tekeze sub-basins:

In this study it is observed that parameters response routine (alfa), capillary rise coefficient (cflux) and recession coefficient for lower reservoir (K<sub>4</sub>) do not show significant

effect on the model performance. Thus, it can be kept as default value when applying HBV model to the next regionalization studies.

In this study multiple linear regression model is the best method consequently not contribute high runoff volume however, some researcher's analyze multiple linear regression model contributes high runoff volume compare to others methods. For next study each regionalization method must be clearly identified.

HBV-96 model calibrated manually by try and error procedure as keeping the other model parameters are constant and one model parameter is changing within the range, so for this study more advanced automatic model calibration techniques could be useful for the next time.

Further recommendation for the concerned body Tekeze river basin is one of the 12<sup>th</sup> river basins in Ethiopian and contributes in hydropower, water supply and irrigation however, most part of sub basins flow gauged catchments are missing or no recorded flow data and no more research's work were done in the previous time, therefore the concerned

body must be follow-up monitoring service for river flow gauged catchments and further research work are motivated in the basin in order to use water resources effectively.

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## Biography



I am **Amare Tadesse Muche**, when I was completed grade 12th, I joined Hawassa University in department of Water Resources and Irrigation Engineering after finishing 5 years study I acquired Bachelor degree in water Resources and Irrigation Engineering. Arba

Minch university employed me as Assistance lecturer at 2014 G.C and in 2017 G.C. I hold my MSc. degree in Hydraulic and Water Resources Engineering and still I am working at Arbaminch Water Technology Institute as senior Lecturer and I also done so many research papers in our Institute and collaborative research engagement for the community as well as the Institute itself.